

On the tracking of nonholonomic systems

SSC-seminar

June 10, 1999

Outline

- Chained form system + problem formulation
- Cascaded approach
- Controller design
- Elegant(!?) proof
- Simulation
- Underactuated ship tracking
- Conclusions

Tracking Problem (state-feedback)

System dynamics:

$$\dot{x}_1 = u_1$$

$$\dot{x}_2 = u_2$$

$$\dot{x}_3 = x_2 u_1$$

$$\vdots$$

$$\dot{x}_n = x_{n-1} u_1$$

Reference dynamics:

$$\dot{x}_{1,r} = u_{1,r}$$

$$\dot{x}_{2,r} = u_{2,r}$$

$$\dot{x}_{3,r} = x_{2,r} u_{1,r}$$

$$\vdots$$

$$\dot{x}_{n,r} = x_{n-1,r} u_{1,r}$$

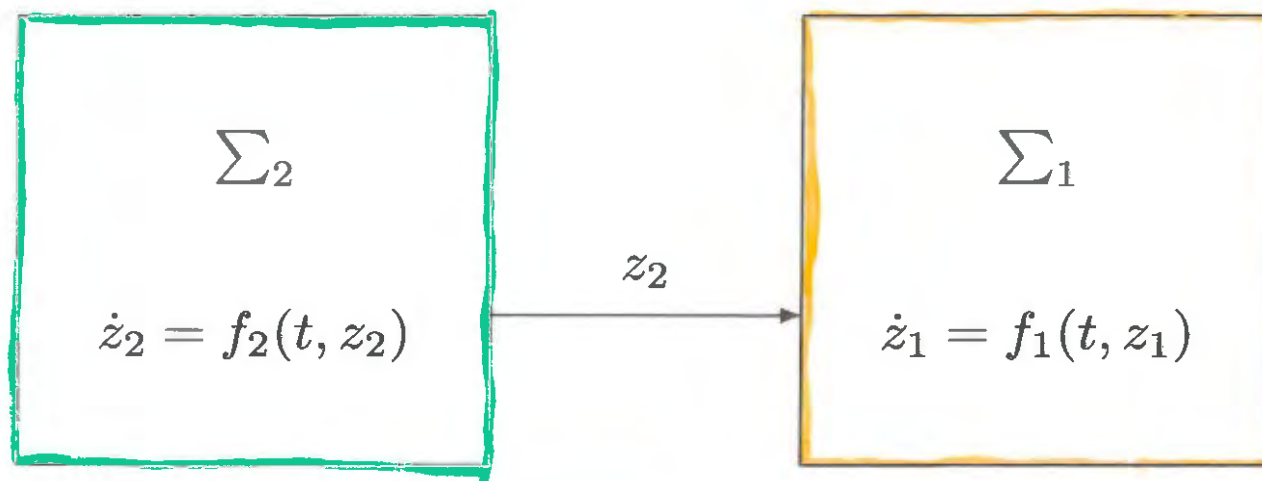
Find control laws

$$u \equiv u(x, x_r, u_r)$$

that yield

$$\lim_{t \rightarrow \infty} |x(t) - x_r(t)| = 0$$

Cascaded systems



$$\dot{z}_1 = f_1(t, z_1) + g(t, z_1, z_2)z_2$$

$$\dot{z}_2 = f_2(t, z_2)$$

Consider the system

$$\begin{aligned}\dot{x}_1 &= -x_1 + x_1^2 x_2 \\ \dot{x}_2 &= -\gamma x_2\end{aligned}$$

Solution:

$$\begin{aligned}x_1(t) &= \frac{2x_1(0)}{x_1(0)x_2(0)e^{-\gamma t} + [2 - x_1(0)x_2(0)]e^{\gamma t}} \\ x_2(t) &= x_2(0)e^{-\gamma t}\end{aligned}$$

When $x_1(0)x_2(0) > 2$ we have a finite escape time

$$t_{esc} = \frac{1}{2\gamma} \ln \frac{x_1(0)x_2(0)}{x_1(0)x_2(0) - 2}$$

Conditions

E. Panteley en A. Loría (S&CL 33(2), 1998):

Cascade Globally Uniformly Asymptotically Stable (GUAS) when

- Σ_1 GUAS, polynomial 'Lyapunov function'
- $g(t, z_1, z_2)$ at most linear in z_1
- Σ_2 GUAS, $z_2(t)$ integrable

Controller Design

Error dynamics ($x_e = x - x_r$):

$$x_{1,e} = u_1 - u_{1,r}$$

$$x_{2,e} = u_2 - u_{2,r}$$

$$\begin{aligned} x_{3,e} &= x_2 u_1 - x_{2,r} u_{1,r} && + x_2 u_{1,r} - x_{2,r} u_{1,r} \\ &= u_{1,r} x_{2,e} + x_2 (u_1 - u_{1,r}) \end{aligned}$$

$$\vdots$$

$$\begin{aligned} x_{n,e} &= x_{n-1} u_1 - x_{n-1,r} u_{1,r} && + x_{n-1} u_{1,r} - x_{n-1,r} u_{1,r} \\ &= u_{1,r} x_{n-1,e} + x_{n-1} (u_1 - u_{1,r}) \end{aligned}$$

Controller Design

Error dynamics ($x_e = x - x_r$):

$$\begin{array}{rclcl} \dot{x}_{2,e} & = & 0 & + & (u_2 - u_{2,r}) & + & 0 \\ \dot{x}_{3,e} & = & u_{1,r}x_{2,e} & + & & + & x_2(u_1 - u_{1,r}) \\ & & \vdots & & & & \vdots \\ \dot{x}_{n,e} & = & u_{1,r}x_{n-1,e} & + & & + & x_{n-1}(u_1 - u_{1,r}) \end{array}$$

$$\dot{x}_{1,e} = (u_1 - u_{1,r})$$

Problem has reduced to (seperately) stabilizing the error-dynamics

$$\begin{bmatrix} \dot{x}_{2,e} \\ \dot{x}_{3,e} \\ \dot{x}_{4,e} \\ \vdots \\ \dot{x}_{n,e} \end{bmatrix} = \begin{bmatrix} 0 & \dots & \dots & \dots & 0 \\ u_{1,r} & \ddots & & & \vdots \\ 0 & u_{1,r} & \ddots & & \vdots \\ \vdots & \ddots & \ddots & \ddots & \vdots \\ 0 & \dots & 0 & u_{1,r} & 0 \end{bmatrix} \begin{bmatrix} x_{2,e} \\ x_{3,e} \\ x_{4,e} \\ \vdots \\ x_{n,e} \end{bmatrix} + \begin{bmatrix} 1 \\ 0 \\ 0 \\ \vdots \\ 0 \end{bmatrix} (u_2 - u_{2,r})$$

and

$$\dot{x}_{1,e} = (u_1 - u_{1,r})$$

Stabilizing the $x_{1,e}$ dynamics:

$$u_1 = u_{1,r} - c_1 x_{1,e} \quad c_1 > 0$$

For stabilizing the $[x_{2,e}, \dots, x_{n,e}]^T$ dynamics we need *uniform controllability*.

This turns out to be the case if and only if the vector

$$\begin{bmatrix} 1 \\ \int_{t_0}^t u_{1,r}(\sigma) d\sigma \\ \vdots \\ \left(\int_{t_0}^t u_{1,r}(\sigma) d\sigma \right)^{n-1} \end{bmatrix}$$

or simpler:
 $\exists \epsilon > 0, \exists \delta > 0$ s.t.
 $\forall t \geq 0 \exists s \in [t, t+\delta]$
s.t. $u_{1,r}(s) \geq \epsilon$

is persistently exciting.

We can use several controllers $u_2 = u_{2,r} - K(t)[x_{2,e}, \dots, x_{n,e}]^T$ for globally exponentially stabilizing

$$\begin{bmatrix} \dot{x}_{2,e} \\ \dot{x}_{3,e} \\ \dot{x}_{4,e} \\ \vdots \\ \dot{x}_{n,e} \end{bmatrix} = \begin{bmatrix} 0 & \dots & \dots & \dots & 0 \\ u_{1,r} & \ddots & & & \vdots \\ 0 & u_{1,r} & \ddots & & \vdots \\ \vdots & \ddots & \ddots & \ddots & \vdots \\ 0 & \dots & 0 & u_{1,r} & 0 \end{bmatrix} \begin{bmatrix} x_{2,e} \\ x_{3,e} \\ x_{4,e} \\ \vdots \\ x_{n,e} \end{bmatrix} + \begin{bmatrix} 1 \\ 0 \\ 0 \\ \vdots \\ 0 \end{bmatrix} (u_2 - u_{2,r})$$

- $K(t) = -B^T \left[\int_t^{t+\delta} 2e^{4\alpha(t-\sigma)} \Phi(t, \sigma) B B^T \Phi^T(t, \sigma) d\sigma \right]^{-1}$
- Pole-placement (cf. Valasek & Olgac, needs $\dot{u}_{1,r}, \dots, \dot{u}_{1,r}^{(n-2)}$)
- $K(t) = \gamma B^T \Phi^{-T}(t, t_0) \Phi^{-1}(t, t_0)$ (M.-S. Chen)

Note that we need $\Phi(t, t_0)$:

$$\Phi(t, t_0) = \begin{bmatrix} f_0(t, t_0) & 0 & \dots & 0 \\ f_1(t, t_0) & f_0(t, t_0) & \ddots & \vdots \\ \vdots & \ddots & \ddots & 0 \\ f_{n-1}(t, t_0) & \dots & f_1(t, t_0) & f_0(t, t_0) \end{bmatrix}$$

where

$$f_k(t, t_0) = \frac{1}{k!} \left[\int_{t_0}^t u_{1,r}(\sigma) d\sigma \right]^k = \frac{1}{k!} [x_{1,r}(t) - x_{1,r}(t_0)]^k$$

However, a simpler controller is given by

- $K(t) = [c_2, c_3 u_{1,r}(t), c_4, c_5 u_{1,r}(t), \dots]$ where c_i are such that $\lambda^{n-1} + c_2 \lambda^{n-2} + \dots + c_{n-1} \lambda + c_n$ is Hurwitz.

Proof

Consider the stability of the differential equation

$$\frac{d^m}{dt^m}y(t) + a_1 \frac{d^{m-1}}{dt^{m-1}}y(t) + \dots + a_{m-1} \frac{d}{dt}y(t) + a_m y(t) = 0 \quad (*)$$

Define Hurwitz-determinants

$$\Delta_i = \begin{vmatrix} a_1 & a_3 & a_5 & \dots & a_{2i-1} \\ 1 & a_2 & a_4 & \dots & a_{2i-2} \\ 0 & a_1 & a_3 & \dots & a_{2i-3} \\ 0 & 1 & a_2 & \dots & a_{2i-4} \\ \vdots & \vdots & \vdots & \vdots & \vdots \\ 0 & 0 & 0 & \dots & a_i \end{vmatrix} \quad (i = 1, \dots, m)$$

The system (*) is GES if and only if $\Delta_i > 0$ for $i = 1, \dots, m$.

If we define

$$b_1 = \Delta_1, \quad b_2 = \frac{\Delta_2}{\Delta_1}, \quad b_3 = \frac{\Delta_3}{\Delta_1 \Delta_2}, \quad b_i = \frac{\Delta_{i-3} \Delta_i}{\Delta_{i-2} \Delta_{i-1}} \quad (i = 4, \dots, m)$$

the system (*) can also be expressed as

$$\dot{w} = \begin{bmatrix} -b_1 & -b_2 & 0 & \dots & 0 \\ 1 & 0 & \ddots & \ddots & \vdots \\ 0 & \ddots & \ddots & \ddots & 0 \\ \vdots & \ddots & \ddots & \ddots & -b_m \\ 0 & \dots & 0 & 1 & 0 \end{bmatrix} w$$

Define

$$V = b_1 w_1^2 + b_1 b_2 w_2^2 + \dots + b_1 b_2 \cdots b_{m-1} w_{m-1}^2 + b_1 b_2 \cdots b_m w_m^2$$

Then

$$\dot{V} = -b_1^2 w_1^2$$

Does there exist a transformation $z = Sw$ that transforms the system

$$\dot{w} = \begin{bmatrix} -b_1 & -b_2 & 0 & \dots & 0 \\ 1 & 0 & \ddots & \ddots & \vdots \\ 0 & \ddots & \ddots & \ddots & 0 \\ \vdots & \ddots & \ddots & \ddots & -b_m \\ 0 & \dots & 0 & 1 & 0 \end{bmatrix} w$$

into

$$\dot{z} = \begin{bmatrix} -a_1 & -a_2 & \dots & \dots & -a_m \\ 1 & 0 & \dots & \dots & 0 \\ 0 & \ddots & \ddots & & \vdots \\ \vdots & \ddots & \ddots & \ddots & \vdots \\ 0 & \dots & 0 & 1 & 0 \end{bmatrix} z$$

Using the same transformation $z = Sw$ we can transform

$$\dot{z} = \begin{bmatrix} -a_1 & -a_2 u_{1,r}(t) & -a_3 & -a_4 u_{1,r}(t) & \dots \\ u_{1,r}(t) & 0 & \dots & \dots & 0 \\ 0 & \ddots & \ddots & & \vdots \\ \vdots & \ddots & \ddots & \ddots & \vdots \\ 0 & \dots & 0 & u_{1,r}(t) & 0 \end{bmatrix} z$$

into

$$\dot{w} = \begin{bmatrix} -b_1 & -b_2 u_{1,r}(t) & 0 & \dots & 0 \\ u_{1,r}(t) & 0 & \ddots & \ddots & \vdots \\ 0 & \ddots & \ddots & \ddots & 0 \\ \vdots & \ddots & \ddots & \ddots & -b_m u_{1,r}(t) \\ 0 & \dots & 0 & u_{1,r}(t) & 0 \end{bmatrix} w$$

Again

$$V = b_1 w_1^2 + b_1 b_2 w_2^2 + \dots + b_1 b_2 \dots b_{m-1} w_{m-1}^2 + b_1 b_2 \dots b_m w_m^2$$

results into

$$\dot{V} = -b_1^2 w_1^2$$

We can conclude GES if the pair

$$\left(\begin{bmatrix} -b_1 & -b_2 u_{1,r}(t) & 0 & \dots & 0 \\ u_{1,r}(t) & 0 & \ddots & \ddots & \vdots \\ 0 & \ddots & \ddots & \ddots & 0 \\ \vdots & \ddots & \ddots & \ddots & -b_m u_{1,r}(t) \\ 0 & \dots & 0 & u_{1,r}(t) & 0 \end{bmatrix}, [b_1, 0, \dots, 0] \right)$$

is uniformly completely observable (UCO).

Corollary from a result by G. Kern (1982)

Assume that $A(t)$ satisfies a Lipschitz condition, i.e.

$$|A(t) - A(t')| \leq L|t - t'| \quad \forall t, t' \leq 0$$

The pair $(A(t), C(t))$ is UCO if there exists $\delta > 0$ and s with $t - \delta \leq s \leq t$ such that $W(t - \delta, t)$ where

$$W(t - \delta, t) \int_t^{t-\delta} e^{A(s)(t-\tau)} C^T(\tau) C(\tau) e^{A^T(s)(t-\tau)} d\tau$$

satisfies

$$0 < \alpha_1(\delta)I \leq W(t - \delta, t) \quad \forall t \leq 0$$

To summarize

The error dynamics

$$\dot{x}_{1,e} = u_1 - u_{1,r}$$

$$\dot{x}_{2,e} = u_2 - u_{2,r}$$

$$\dot{x}_{3,e} = x_2 u_1 - x_{2,r} u_{1,r}$$

$$\vdots$$

$$\dot{x}_{n,e} = x_{n-1} u_1 - x_{n-1,r} u_{1,r}$$

in closed loop with the controller

$$u_1 = u_{1,r} - c_1 x_{1,e}$$

$$u_2 = u_{2,r} - K(t)[x_{2,e}, \dots, x_{n,e}]^T$$

is globally (K -exponentially) asymptotically stable.

Simulations

Car pulling a single trailer:

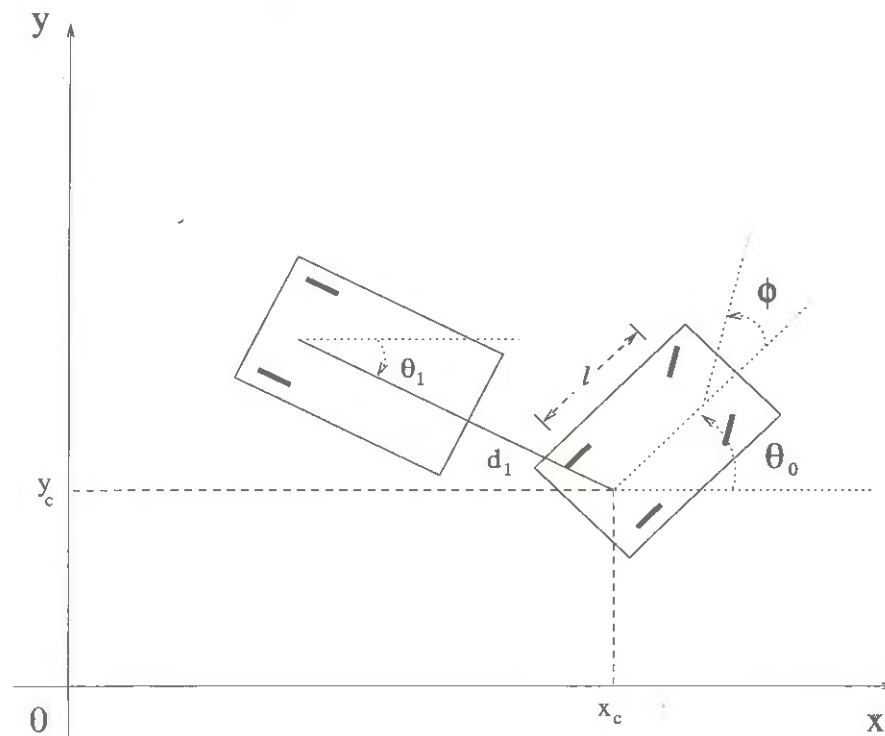
$$\dot{x}_c = v \cos \theta_0$$

$$\dot{y}_c = v \sin \theta_0$$

$$\dot{\phi} = \omega$$

$$\dot{\theta}_0 = \frac{1}{l} v \tan \phi$$

$$\dot{\theta}_1 = \frac{1}{d_1} v \sin(\theta_0 - \theta_1)$$



Moving along a straight line:

$$u_{1,r} = 1 \quad u_{2,r} = 0$$

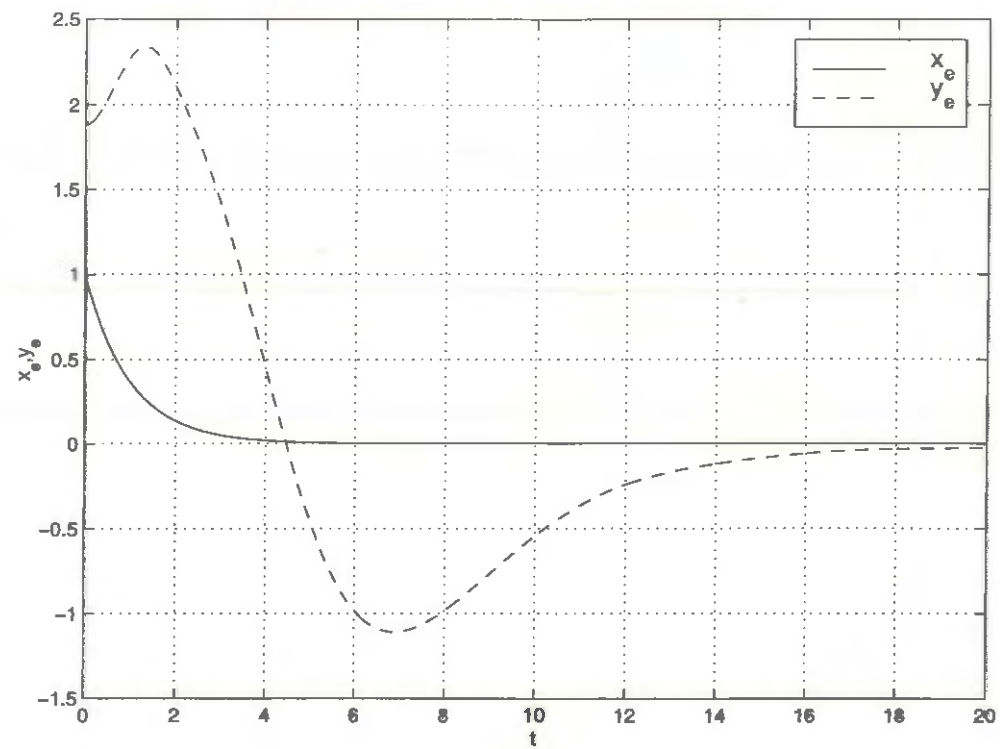
with initial conditions

$$x_{ir}(0) = 0 \quad (i = 1, \dots, 5) \quad x_1(0) = 1, \quad x_j(0) = 0.5 \quad (j = 2, \dots, 5)$$

controller polynomial: poles in -2

observer polynomial: poles in -3 .

State-feedback



Saturated control

Problem has reduced to stabilizing the error-dynamics

$$\begin{bmatrix} \dot{x}_{2,e} \\ \dot{x}_{3,e} \\ \dot{x}_{4,e} \\ \vdots \\ \dot{x}_{n,e} \end{bmatrix} = \begin{bmatrix} 0 & \dots & \dots & \dots & 0 \\ u_{1,r} & \ddots & & & \vdots \\ 0 & u_{1,r} & \ddots & & \vdots \\ \vdots & \ddots & \ddots & \ddots & \vdots \\ 0 & \dots & 0 & u_{1,r} & 0 \end{bmatrix} \begin{bmatrix} x_{2,e} \\ x_{3,e} \\ x_{4,e} \\ \vdots \\ x_{n,e} \end{bmatrix} + \begin{bmatrix} 1 \\ 0 \\ 0 \\ \vdots \\ 0 \end{bmatrix} (u_2 - u_{2,r})$$

and

$$\dot{x}_{1,e} = (u_1 - u_{1,r})$$

We can also use $u_1 = u_{1,r} - \text{sat}(x_{1,e})$.

Saturated controller:

$$\begin{aligned}u_{1,sat} &= u_{1,r} - \sigma(x_{1,e}) \\u_{2,sat} &= u_{2,r} - \sum_{k=1}^4 \epsilon^k \sigma(y_k)\end{aligned}$$

where

$$\begin{bmatrix} y_1 \\ y_2 \\ y_3 \\ y_4 \end{bmatrix} = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 1 & \epsilon & 0 & 0 \\ 1 & \epsilon^2 + \epsilon & \epsilon & 0 \\ 1 & \epsilon^3 + \epsilon^2 + \epsilon & \epsilon^5 + \epsilon^4 + \epsilon^3 & \epsilon^6 \end{bmatrix} \begin{bmatrix} x_{2,e} \\ x_{3,e} \\ x_{4,e} \\ x_{5,e} \end{bmatrix}$$

Ship-dynamics

$$\dot{x} = u \cos \psi - v \sin \psi$$

$$\dot{y} = u \sin \psi + v \cos \psi$$

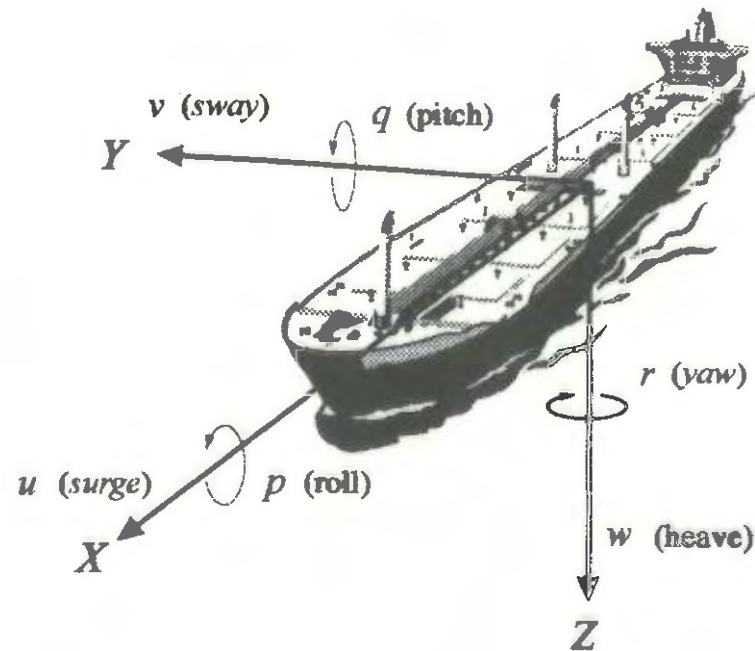
$$\dot{\psi} = r$$

$$\dot{u} = \tau_u$$

$$\dot{v} = -c u r - d v$$

$$\dot{r} = \tau_r$$

where $c, d > 0$



Using

$$x_1 = u$$

$$x_2 = v$$

$$x_3 = x \cos \psi + y \sin \psi$$

$$x_4 = x \sin \psi + y \cos \psi$$

$$x_5 = z_r$$

$$x_6 = \psi$$

we obtain

$$\dot{x}_1 = \tau_u$$

$$\dot{x}_2 = -cx_1x_5 - dx_2$$

$$\dot{x}_3 = x_1 + x_4x_5$$

$$\dot{x}_4 = x_2 - x_3x_5$$

$$\dot{x}_5 = \tau_r$$

$$\dot{x}_6 = x_5$$

Tracking Problem

System dynamics:

$$\dot{x}_1 = \tau_u$$

$$\dot{x}_2 = -cx_1x_5 - dx_2$$

$$\dot{x}_3 = x_1 + x_4x_5$$

$$\dot{x}_4 = x_2 - x_3x_5$$

$$\dot{x}_5 = \tau_r$$

$$\dot{x}_6 = x_5$$

Reference dynamics:

$$\dot{x}_{1,d} = \tau_{u,d}$$

$$\dot{x}_{2,d} = -cx_{1,d}x_{5,d} - dx_{2,d}$$

$$\dot{x}_{3,d} = x_{1,d} + x_{4,d}x_{5,d}$$

$$\dot{x}_{4,d} = x_{2,d} - x_{3,d}x_{5,d}$$

$$\dot{x}_{5,d} = \tau_{r,d}$$

$$\dot{x}_{6,d} = x_{5,d}$$

Find control laws

$$\tau \equiv \tau(x, x_d, \tau_d)$$

that yield

$$\lim_{t \rightarrow \infty} |x(t) - x_d(t)| = 0$$

Tracking error dynamics:

$$\begin{aligned}
 \begin{bmatrix} \dot{x}_{1,e} \\ \dot{x}_{2,e} \\ \dot{x}_{3,e} \\ \dot{x}_{4,e} \end{bmatrix} &= \begin{bmatrix} 0 & 0 & 0 & 0 \\ -cx_{5,d}(t) & -d & 0 & 0 \\ 1 & 0 & 0 & x_{5,d}(t) \\ 0 & 1 & -x_{5,d} & 0 \end{bmatrix} \begin{bmatrix} x_{1,e} \\ x_{2,e} \\ x_{3,e} \\ x_{4,e} \end{bmatrix} + \\
 &+ \begin{bmatrix} 1 \\ 0 \\ 0 \\ 0 \end{bmatrix} (\tau_u - \tau_{u,d}) + \begin{bmatrix} 0 & 0 \\ -cx_1 & 0 \\ x_4 & 0 \\ -x_3 & 0 \end{bmatrix} \begin{bmatrix} x_{5,e} \\ x_{6,e} \end{bmatrix} \\
 \begin{bmatrix} \dot{x}_{5,e} \\ \dot{x}_{6,e} \end{bmatrix} &= \begin{bmatrix} 0 & 0 \\ 1 & 0 \end{bmatrix} \begin{bmatrix} x_{5,e} \\ x_{6,e} \end{bmatrix} + \begin{bmatrix} 1 \\ 0 \end{bmatrix} (\tau_r - \tau_{r,d})
 \end{aligned}$$

Assume that $x_{1,d}$, $x_{3,d}$ and $x_{4,d}$ are bounded and that $x_{5,d}(t) \not\rightarrow 0$.

Then for the state-feedback problem we can use the controller

$$\begin{aligned}\tau_u &= \tau_{u,d} - k_1 x_{1,e} + k_2 x_{5,d}(t) x_{2,e} - k_3 x_{3,e} + k_4 x_{5,d}(t) x_{4,e} \\ \tau_r &= \tau_{r,d} - k_5 x_{5,e} - k_6 x_{6,e}\end{aligned}$$

If additionally $x_{5,d}(t)$ is bounded

Then for the output-feedback problem we can use the controller

$$\begin{aligned}\tau_u &= \tau_{u,d} - k_1 \hat{x}_{1,e} + k_2 x_{5,d}(t) \hat{x}_{2,e} - k_3 \hat{x}_{3,e} + k_4 x_{5,d}(t) \hat{x}_{4,e} \\ \tau_r &= \tau_{r,d} - k_5 \hat{x}_{5,e} - k_6 \hat{x}_{6,e}\end{aligned}$$

$\hat{x}$ is generated from the observer

$$\hat{x}_{1e-4e} = A(t)\hat{x}_{1e-4e} + B(\tau_u - \tau_{u,d}) + L(t)(y_{1-2} - \hat{y}_{1-2})$$

$$\hat{y}_{1-2} = C\hat{x}_{1e-4e}$$

$$\hat{x}_{5e-6e} = \bar{A}\hat{x}_{5e-6e} + \bar{B}(\tau_r - \tau_{r,d}) + \bar{L}(y_3 - \hat{y}_3)$$

$$\hat{y}_3 = \bar{C}\hat{x}_{5e-6e}$$

where

$$L(t) = \begin{bmatrix} l_{11} & 0 \\ 0 & l_{22} \\ l_{31} & x_{5,d}(t) \\ -x_{5,d}(t) & l_{42} \end{bmatrix} \quad \bar{L} = [l_5 \ l_6]$$

Conclusions

- Linear (time-varying) controllers for nonlinear chained form system.
- Separate controller design by viewing the system as a cascade.
- Both state and output feedback.
- Global results (not based on linearization)
- Similar approach can be used with saturated control inputs.
- Cascaded approach works for ship too!