Globally bounded tracking controllers for rigid robot systems

European Control Conference ECC'97 3 July 1997, Brussels, Belgium

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Rigid robot manipulator

A rigid robot manipulator with revolute joints can be described as

$$M(q)\ddot{q} + C(q,\dot{q})\dot{q} + G(q) = \tau \tag{1}$$

 $q n \times 1$ vector of joint displacements

 τ $n \times 1$ vector of applied torques

M(q) $n \times n$ manipulator inertia matrix

 $C(q,\dot{q})\dot{q}$ $n \times 1$ vector of centripetal and Coriolis torques

G(q) $n \times 1$ vector of gravitational torques

Problem formulation

Design a controller for τ that globally steers the system

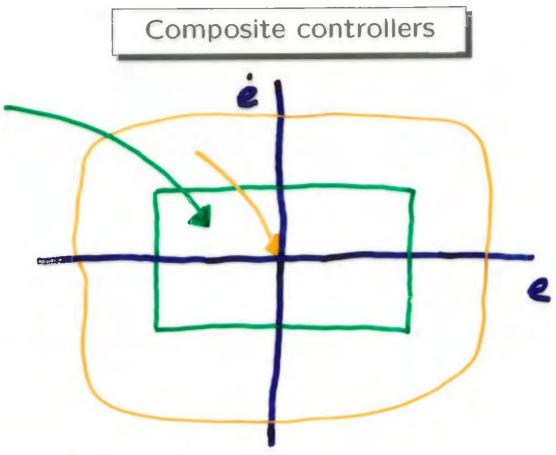
$$M(q)\ddot{q} + C(q,\dot{q})\dot{q} + G(q) = \tau$$

towards any desired trajectory $q_d(t) \in C^2$ under the input limitations

$$| au_i(t)| \leq au_{max,i}$$

provided q_d satisfies

$$||q_d(t)|| \le B_0 \quad ||\dot{q}_d(t)|| \le B_1 \quad ||\ddot{q}_d(t)|| \le B_2$$



Approach used:

 Find tracking controller whose region of attraction contains the set

$$\{(e,\dot{e}) \mid ||e|| \leq B_0 \wedge ||\dot{e}|| \leq B_1\}$$
 where $e \equiv q-q_d.$

- Find globally bounded regulating controller.
- · Combine both controllers.

The classes \mathcal{F}^n and \mathcal{B}^n

Definition of \mathcal{F}^n :

All continuous functions $f: I\!\!R^n \to I\!\!R^n$ for which there exists an $F: I\!\!R^n \to I\!\!R$ such that

$$f(x) = \frac{\partial F}{\partial x}(x) = \begin{bmatrix} \frac{\partial F}{\partial x_1}(x_1, \dots, x_n) \\ \vdots \\ \frac{\partial F}{\partial x_n}(x_1, \dots, x_n) \end{bmatrix}$$

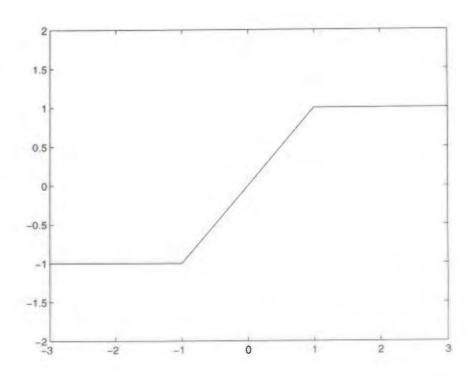
and for which $x^T f(x)$ is positive definite.

Definition of \mathcal{B}^n :

$$\mathcal{B}^n \triangleq \mathcal{F}^n \cap L_\infty$$

Examples:

- $f(x) = \Lambda[f_1(x), \dots, f_n(x)]^T$ where f_i non-decreasing with $f_i(0) = 0$ and $\Lambda = \Lambda^T > 0$ diagonal.
- f(x) = Kx where $K = K^T > 0$.



Globally tracking controllers

The control law

$$\tau = M(q)\ddot{q}_d + C(q, \dot{q})\dot{q}_d + G(q) - \mathbf{k}_0 f_1(\dot{e}) - \mathbf{k}_0 f_2(e)$$

where $e \equiv q - q_d$ results in the closed-loop system

$$M(q)\ddot{e} + C(q,\dot{q})\dot{e} + f_1(\dot{e}) + f_2(e) = 0.$$

Proposition If $f_1 \in C^1$, $f_2 \in C^2$, $\frac{\partial f_2}{\partial e}(0) > 0$ then (*) is globally asymptotically stable.

Corollary If q_d is a fixed point then (**) is globally asymptotically stable. (f. \$ 60°)

Note that in case q_d is a fixed point the controller reduces to

$$\tau = G(q) - \mathbf{N} f_1(\dot{e}) - \mathbf{N} f_2(e)$$

which for $f_1, f_2 \in \mathcal{B}^n$ is bounded.

Proof Consider the candidate Lyapunov function

$$V(t, e, \dot{e}) = \frac{1}{2}\dot{e}^{T}M(q)\dot{e} + F_{2}(e)$$

It's time-derivative along (1) becomes

$$\underline{\dot{V}(t,e,\dot{e})} = \dot{e}^{T}M(q)\ddot{e} + \frac{1}{2}\dot{e}^{T}\dot{M}(q)\dot{e} + \dot{e}^{T}f_{2}(e)
= \dot{e}^{T}[-C(q,\dot{q})\dot{e} - f_{1}(\dot{e})] + \frac{1}{2}\dot{e}^{T}\dot{M}(q)\dot{e}
= \dot{e}^{T}[\frac{1}{2}\dot{M}(q) - C(q,\dot{q})]\dot{e} - \dot{e}^{T}f_{1}(\dot{e})
= -\dot{e}^{T}f_{1}(\dot{e})$$

which is negative semi-definite in (e, \dot{e}) .

Finish the proof of the proposition using Matrosov's Theorem, where

$$W(t,e,\dot{e}) = \ddot{V}(t,e,\dot{e})$$

Finish the proof of the corollary using <u>LaSalle</u>'s invariance principle.

Composite controllers that solve the bounded globally tracking problem (I)

Consider the system (1). Then there exists a switching time $t_s \geq 0$ such that given any $\tilde{t}_s \geq t_s$ the composite controller

$$\tau = \begin{cases} G(q) - f_1(\dot{q}) - f_2(q) & t < \tilde{t}_s \\ M(q)\ddot{q}_d + C(q, \dot{q})\dot{q}_d + G(q) - f_3(\dot{e}) - f_4(e) & t \ge \tilde{t}_s \end{cases}$$
(3)

results in a globally asymptotically stable closedloop system.

Furthermore, if $f_1, f_2 \in \mathcal{B}^n$ we can determine a τ_{max} such that the controller (3) satisfies

$$||\tau(t)|| \leq \tau_{max} \quad \forall t \geq 0.$$

Composite controllers that solve the bounded globally tracking problem (II)

Consider the system (1). Then there exists a switching time $t_s>0$ and a $\Delta>0$ such that the controller

$$\tau = [1 - s_{\Delta}(t - t_s)]\tau_1 + s_{\Delta}(t - t_s)\tau_2$$

where

$$\tau_1 = G(q) - \mathbf{K} f_1(\dot{q}) - \mathbf{K} f_2(\underline{q})$$

$$\tau_2 = M(q) \ddot{q}_d + C(q, \dot{q}) \dot{q}_d + G(q) - \mathbf{K} f_2(\dot{e}) - \mathbf{K} f_2(\dot{e})$$
results in a globally asymptotically stable closed-loop system.

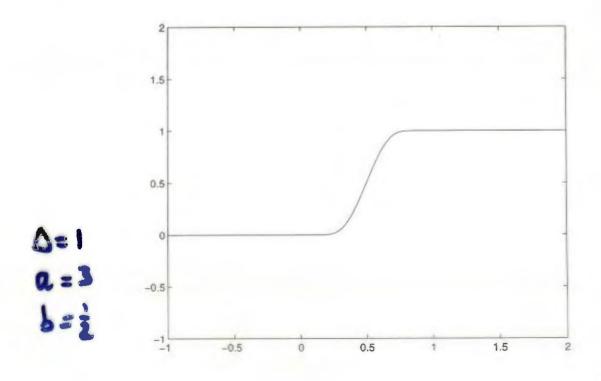
Here $s_{\Delta}: I\!\!R \to I\!\!R$ is a smooth nondecreasing function such that

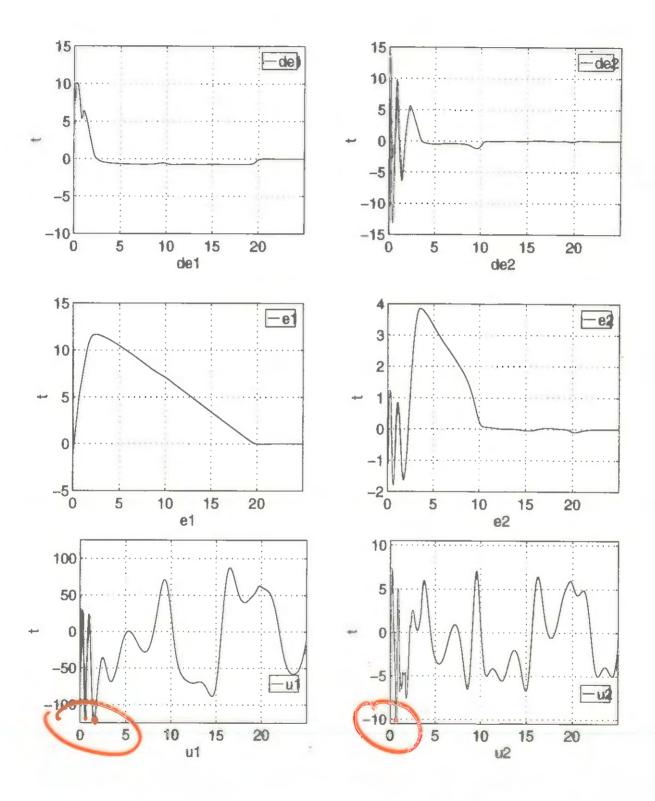
$$s_{\Delta}(x) = \begin{cases} 0 & x \leq 0 \\ \dots & 0 < x < \Delta \\ 1 & \Delta \leq x \end{cases}$$

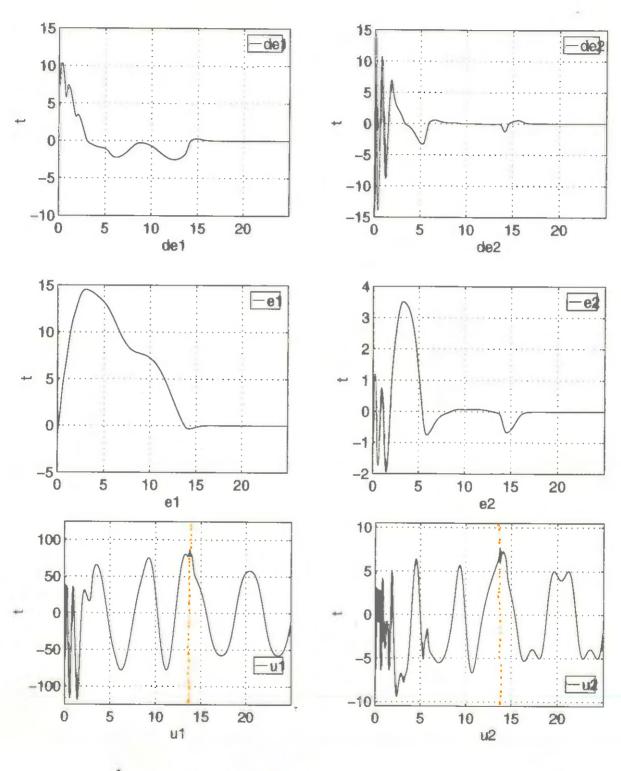
Examples of such $s_{\Delta}(x) \in C^{\infty}$ are given by:

$$\begin{cases} \frac{1}{2} \exp \left[\frac{a}{x(x-b)} - \frac{a}{\frac{1}{2}\Delta(\frac{1}{2}\Delta - b)} \right] & 0 < x \le \frac{1}{2}\Delta \\ 1 - \frac{1}{2} \exp \left[\frac{a}{(x-\Delta)(x-\Delta + b)} - \frac{a}{\frac{1}{2}\Delta(\frac{1}{2}\Delta - b)} \right] & \frac{1}{2}\Delta < x < \Delta \\ 1 & \Delta \le x \end{cases}$$

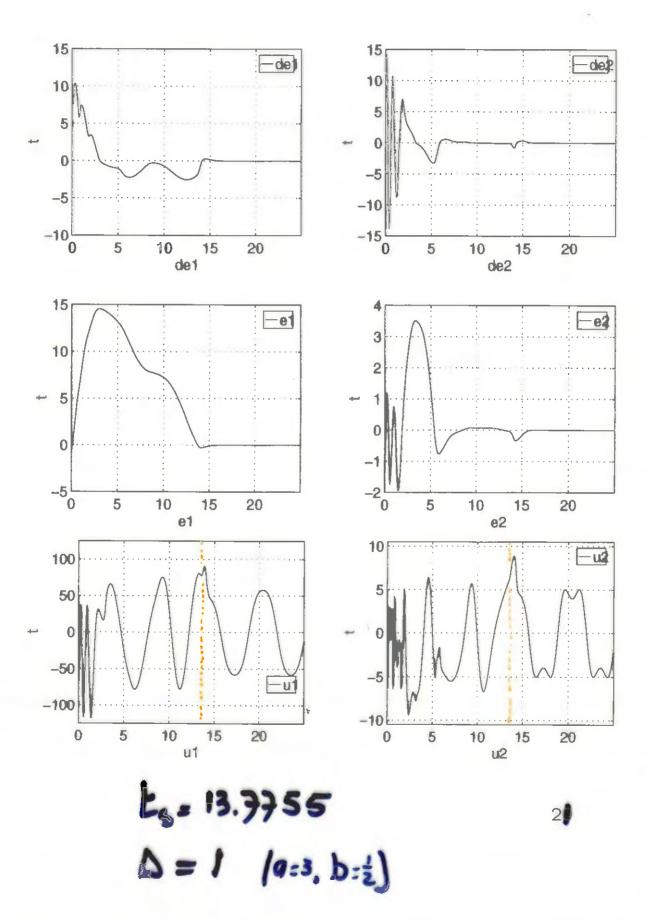
where a > 0, $b \ge \Delta > 0$.







ts = 13.7755



Controller used:

$$\tau = M(q) \ddot{q}_d + C(q,\dot{q}) \dot{q}_d + G(q) - K_p e - K_d \dot{e}$$
 where

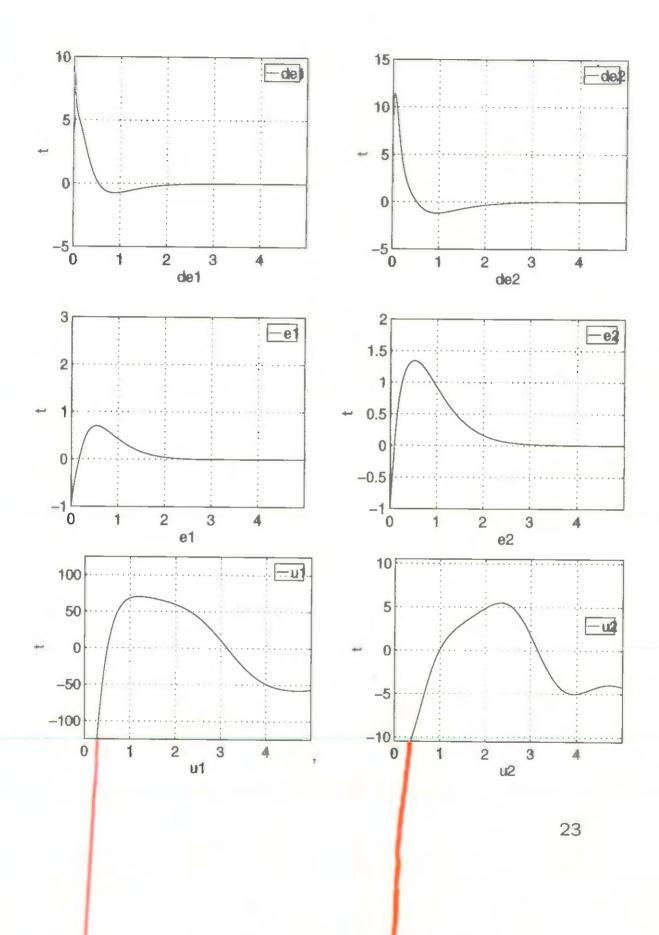
$$K_p = \begin{bmatrix} 76 & 0 \\ 0 & 6.0 \end{bmatrix} \qquad K_d = \begin{bmatrix} 50 & 0 \\ 0 & 5.1 \end{bmatrix}$$

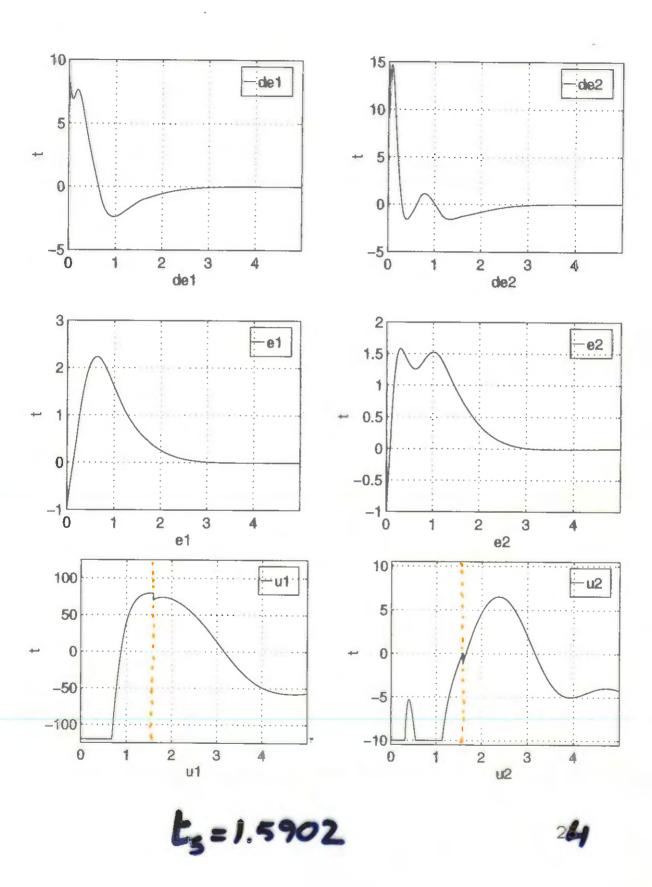
Composite controller:

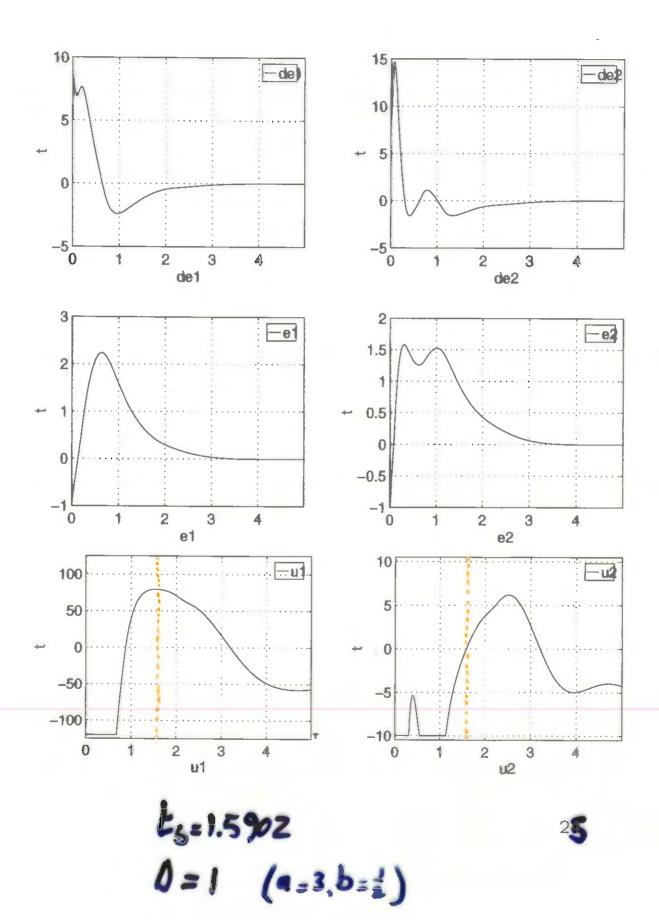
$$\tau = \mathsf{Sat}(G(q) - K_p e - K_d \dot{e})$$

until $V_2(t, e, \dot{e}) \leq 20$. From then on:

$$\tau = M(q)\ddot{q}_d + C(q,\dot{q})\dot{q}_d + G(q) - K_p e - K_d \dot{e}$$







Conclusions

- Composite controllers can solve the globally bounded tracking control problem, not only for rigid robot systems.
- A drawback still exists in the time-varying nature of the composite controller.
- How to obtain the best performance possible within prespecified bounds on the input, is an interesting question for further research.